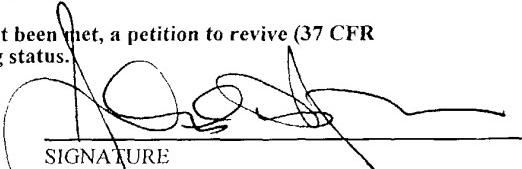


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EPA/PCTO-1390 (Modified) (REV 11-2000)		U S DEPARTMENT OF COMMERCE PATENT AND TRADEMARK OFFICE	
TRANSMITTAL LETTER TO THE UNITED STATES DESIGNATED/ELECTED OFFICE (DO/EO/US) CONCERNING A FILING UNDER 35 U.S.C. 371		ATTORNEY'S DOCKET NUMBER WEI0035	
INTERNATIONAL APPLICATION NO. PCT/EP00/07987	INTERNATIONAL FILING DATE 16 August 2000 (16/08/2000)	U S APPLICATION NO (IF KNOWN, SEE 37 CFR 10/049902	
TITLE OF INVENTION SKULL POT FOR MELTING OR REFINING INORGANIC SUBSTANCES, ESPECIALLY GLASSES AND GLASS CERAMICS		PRIORITY DATE CLAIMED 21 August 1999 (21/08/1999)	
APPLICANT(S) FOR DO/EO/US ROMER, Hildegard et al.			
Applicant herewith submits to the United States Designated/Elected Office (DO/EO/US) the following items and other information:			
<ol style="list-style-type: none">1. <input checked="" type="checkbox"/> This is a FIRST submission of items concerning a filing under 35 U.S.C. 371.2. <input type="checkbox"/> This is a SECOND or SUBSEQUENT submission of items concerning a filing under 35 U.S.C. 371.3. <input checked="" type="checkbox"/> This is an express request to begin national examination procedures (35 U.S.C. 371(f)) The submission must include items (5), (6), (9) and (24) indicated below.4. <input checked="" type="checkbox"/> The US has been elected by the expiration of 19 months from the priority date (Article 31).5. <input checked="" type="checkbox"/> A copy of the International Application as filed (35 U.S.C. 371 (c) (2))<ol style="list-style-type: none">a. <input checked="" type="checkbox"/> is attached hereto (required only if not communicated by the International Bureau).b. <input type="checkbox"/> has been communicated by the International Bureau.c. <input type="checkbox"/> is not required, as the application was filed in the United States Receiving Office (RO/US).6. <input checked="" type="checkbox"/> An English language translation of the International Application as filed (35 U.S.C. 371(c)(2)).<ol style="list-style-type: none">a. <input checked="" type="checkbox"/> is attached hereto.b. <input type="checkbox"/> has been previously submitted under 35 U.S.C. 154(d)(4).7. <input type="checkbox"/> Amendments to the claims of the International Application under PCT Article 19 (35 U.S.C. 371 (c)(3))<ol style="list-style-type: none">a. <input type="checkbox"/> are attached hereto (required only if not communicated by the International Bureau)b. <input type="checkbox"/> have been communicated by the International Bureau.c. <input type="checkbox"/> have not been made; however, the time limit for making such amendments has NOT expired.d. <input type="checkbox"/> have not been made and will not be made.8. <input type="checkbox"/> An English language translation of the amendments to the claims under PCT Article 19 (35 U.S.C. 371(c)(3)).9. <input checked="" type="checkbox"/> An oath or declaration of the inventor(s) (35 U.S.C. 371 (c)(4)).10. <input type="checkbox"/> An English language translation of the annexes to the International Preliminary Examination Report under PCT Article 36 (35 U.S.C. 371 (c)(5)).11. <input checked="" type="checkbox"/> A copy of the International Preliminary Examination Report (PCT/IPEA/409).12. <input checked="" type="checkbox"/> A copy of the International Search Report (PCT/ISA/210).			
Items 13 to 20 below concern document(s) or information included:			
<ol style="list-style-type: none">13. <input checked="" type="checkbox"/> An Information Disclosure Statement under 37 CFR 1.97 and 1.98.14. <input type="checkbox"/> An assignment document for recording. A separate cover sheet in compliance with 37 CFR 3.28 and 3.31 is included15. <input checked="" type="checkbox"/> A FIRST preliminary amendment16. <input type="checkbox"/> A SECOND or SUBSEQUENT preliminary amendment17. <input type="checkbox"/> A substitute specification18. <input type="checkbox"/> A change of power of attorney and/or address letter19. <input type="checkbox"/> A computer-readable form of the sequence listing in accordance with PCT Rule 13ter 2 and 35 U.S.C. 1821 - 182520. <input type="checkbox"/> A second copy of the published international application under 35 U.S.C. 154(d)(4)21. <input type="checkbox"/> A second copy of the English language translation of the international application under 35 U.S.C. 154(d)(4)22. <input checked="" type="checkbox"/> Certificate of Mailing by Express Mail23. <input checked="" type="checkbox"/> Other items or information: Check No. <u>102863</u>			

APPLICATION NO. (IF KNOWN) SEE BACK	INTERNATIONAL APPLICATION NO PCT/EP00/07987	ATTORNEY'S DOCKET NUMBER WEI0035																																						
<p>24. The following fees are submitted</p> <p>BASIC NATIONAL FEE (37 CFR 1.492 (a) (1) - (5)) :</p> <table border="0" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 80%;"><input type="checkbox"/> Neither international preliminary examination fee (37 CFR 1.482) nor international search fee (37 CFR 1.445(a)(2)) paid to USPTO and International Search Report not prepared by the EPO or JPO</td> <td style="width: 20%; text-align: right;">\$1040.00</td> </tr> <tr> <td><input checked="" type="checkbox"/> International preliminary examination fee (37 CFR 1.482) not paid to USPTO but International Search Report prepared by the EPO or JPO</td> <td style="text-align: right;">\$890.00</td> </tr> <tr> <td><input type="checkbox"/> International preliminary examination fee (37 CFR 1.482) not paid to USPTO but international search fee (37 CFR 1.445(a)(2)) paid to USPTO</td> <td style="text-align: right;">\$740.00</td> </tr> <tr> <td><input type="checkbox"/> International preliminary examination fee (37 CFR 1.482) paid to USPTO but all claims did not satisfy provisions of PCT Article 33(1)-(4)</td> <td style="text-align: right;">\$710.00</td> </tr> <tr> <td><input type="checkbox"/> International preliminary examination fee (37 CFR 1.482) paid to USPTO and all claims satisfied provisions of PCT Article 33(1)-(4)</td> <td style="text-align: right;">\$100.00</td> </tr> </table> <p style="text-align: center;">ENTER APPROPRIATE BASIC FEE AMOUNT =</p> <p style="text-align: right;">\$890.00</p> <p>Surcharge of \$130.00 for furnishing the oath or declaration later than months from the earliest claimed priority date (37 CFR 1.492 (e)).</p> <table border="0" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 80%;"><input type="checkbox"/> 20 <input type="checkbox"/> 30</td> <td style="width: 20%; text-align: right;">\$0.00</td> </tr> </table>		<input type="checkbox"/> Neither international preliminary examination fee (37 CFR 1.482) nor international search fee (37 CFR 1.445(a)(2)) paid to USPTO and International Search Report not prepared by the EPO or JPO	\$1040.00	<input checked="" type="checkbox"/> International preliminary examination fee (37 CFR 1.482) not paid to USPTO but International Search Report prepared by the EPO or JPO	\$890.00	<input type="checkbox"/> International preliminary examination fee (37 CFR 1.482) not paid to USPTO but international search fee (37 CFR 1.445(a)(2)) paid to USPTO	\$740.00	<input type="checkbox"/> International preliminary examination fee (37 CFR 1.482) paid to USPTO but all claims did not satisfy provisions of PCT Article 33(1)-(4)	\$710.00	<input type="checkbox"/> International preliminary examination fee (37 CFR 1.482) paid to USPTO and all claims satisfied provisions of PCT Article 33(1)-(4)	\$100.00	<input type="checkbox"/> 20 <input type="checkbox"/> 30	\$0.00	CALCULATIONS PTO USE ONLY																										
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<table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="width: 25%;">CLAIMS</th> <th style="width: 25%;">NUMBER FILED</th> <th style="width: 25%;">NUMBER EXTRA</th> <th style="width: 25%;">RATE</th> </tr> </thead> <tbody> <tr> <td>Total claims</td> <td>14 - 20 =</td> <td>0</td> <td>x \$18.00 \$0.00</td> </tr> <tr> <td>Independent claims</td> <td>1 - 3 =</td> <td>0</td> <td>x \$84.00 \$0.00</td> </tr> <tr> <td colspan="3">Multiple Dependent Claims (check if applicable).</td> <td style="text-align: right;"><input type="checkbox"/> \$0.00</td> </tr> <tr> <td colspan="3">TOTAL OF ABOVE CALCULATIONS</td> <td style="text-align: right;">\$890.00</td> </tr> </tbody> </table> <p><input type="checkbox"/> Applicant claims small entity status. See 37 CFR 1.27). The fees indicated above are reduced by 1/2.</p> <table border="0" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 80%;">SUBTOTAL</td> <td style="width: 20%; text-align: right;">\$890.00</td> </tr> </table> <p>Processing fee of \$130.00 for furnishing the English translation later than months from the earliest claimed priority date (37 CFR 1.492 (f))</p> <table border="0" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 80%;"><input type="checkbox"/> 20 <input type="checkbox"/> 30</td> <td style="width: 20%; text-align: right;">\$0.00</td> </tr> </table> <table border="0" style="width: 100%; border-collapse: collapse;"> <tr> <td colspan="2">TOTAL NATIONAL FEE</td> <td style="text-align: right;">\$890.00</td> </tr> </table> <p>Fee for recording the enclosed assignment (37 CFR 1.21(h)). The assignment must be accompanied by an appropriate cover sheet (37 CFR 3.28, 3.31) (check if applicable).</p> <table border="0" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 80%;"><input type="checkbox"/> \$0.00</td> <td style="width: 20%;"></td> </tr> </table> <table border="0" style="width: 100%; border-collapse: collapse;"> <tr> <td colspan="2">TOTAL FEES ENCLOSED</td> <td style="text-align: right;">\$890.00</td> </tr> </table> <table border="0" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 80%;"></td> <td style="width: 20%; text-align: right;">Amount to be: refunded</td> <td style="width: 20%; text-align: right;">\$</td> </tr> <tr> <td></td> <td style="text-align: right;">charged</td> <td style="text-align: right;">\$</td> </tr> </table>		CLAIMS	NUMBER FILED	NUMBER EXTRA	RATE	Total claims	14 - 20 =	0	x \$18.00 \$0.00	Independent claims	1 - 3 =	0	x \$84.00 \$0.00	Multiple Dependent Claims (check if applicable).			<input type="checkbox"/> \$0.00	TOTAL OF ABOVE CALCULATIONS			\$890.00	SUBTOTAL	\$890.00	<input type="checkbox"/> 20 <input type="checkbox"/> 30	\$0.00	TOTAL NATIONAL FEE		\$890.00	<input type="checkbox"/> \$0.00		TOTAL FEES ENCLOSED		\$890.00		Amount to be: refunded	\$		charged	\$	
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<p>a. <input checked="" type="checkbox"/> A check in the amount of \$890.00 to cover the above fees is enclosed.</p> <p>b. <input type="checkbox"/> Please charge my Deposit Account No. _____ in the amount of _____ to cover the above fees. A duplicate copy of this sheet is enclosed.</p> <p>c. <input checked="" type="checkbox"/> The Commissioner is hereby authorized to charge any additional fees which may be required, or credit any overpayment to Deposit Account No. 02-0385 A duplicate copy of this sheet is enclosed.</p> <p>d. <input type="checkbox"/> Fees are to be charged to a credit card. WARNING: Information on this form may become public. Credit card information should not be included on this form. Provide credit card information and authorization on PTO-2038.</p>																																								
<p>NOTE: Where an appropriate time limit under 37 CFR 1.494 or 1.495 has not been met, a petition to revive (37 CFR 1.137(a) or (b)) must be filed and granted to restore the application to pending status.</p> <p>SEND ALL CORRESPONDENCE TO:</p> <p>John F. Hoffman BAKER & DANIELS 111 East Wayne Street, Suite 800 Fort Wayne, Indiana 46802</p> <p>TX: (260) 424-8000 FAX: (260) 460-1700</p>																																								
 SIGNATURE JOHN F. HOFFMAN NAME 26,280 REGISTRATION NUMBER February 19, 2002 DATE																																								

10/049952

IN THE UNITED STATES PATENT AND TRADEMARK OFFICE
19 FEB 2002

In re Application of)
Hildegard Römer et al.) Group:
Serial No.:)
Filed:) Examiner:
Title: SKULL POT FOR MELTING OR REFINING)
INORGANIC SUBSTANCES, ESPECIALLY)
GLASSES AND GLASS CERAMICS)

PRELIMINARY AMENDMENT DELETING
MULTIPLE DEPENDENT CLAIMS

Assistant Commissioner of Patents
Washington, DC 20231

Sir:

Prior to calculating the filing fee, please enter the following amendments to the application.

IN THE CLAIMS

In claim 3, line 1, delete "or 2".

In claim 5, line 1, delete "any one of Claims 1 through 4" and substitute therefor --claim 1--.

In claim 6, line 1, delete "any one of Claims 1 through 5" and substitute therefor --claim 1--.

Please add the following new claims:

7. A skull crucible as claimed in claim 2, characterized in that the sleeve (4) is assigned a device for adjusting or regulating its temperature.

8. A skull crucible as claimed in claim 2, characterized by the following features:

the sleeve (4) has two coaxial sleeves;
the outer sleeve is a metal jacket;
the inner sleeve is a quartz glass tube.

9. A skull crucible as claimed in claim 3, characterized by the following features:

the sleeve (4) has two coaxial sleeves;
the outer sleeve is a metal jacket;
the inner sleeve is a quartz glass tube.

10. A skull crucible as claimed in claim 4, characterized by the following features:

the sleeve (4) has two coaxial sleeves;
the outer sleeve is a metal jacket;
the inner sleeve is a quartz glass tube.

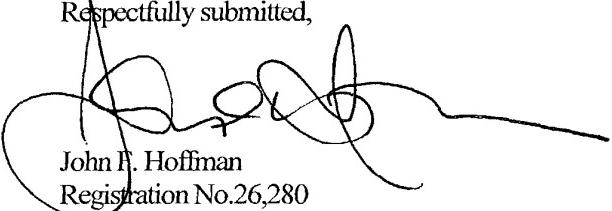
11. A skull crucible as claimed in claim 2, characterized in that the sleeve is height-adjustable.

12. A skull crucible as claimed in claim 3, characterized in that the sleeve is height-adjustable.

John F. Hoffman
Registration No. 26,280

13. A skull crucible as claimed in claim 4, characterized in that the sleeve is height-adjustable.
14. A skull crucible as claimed in claim 5, characterized in that the sleeve is height-adjustable.—

Respectfully submitted,



John F. Hoffman
Registration No. 26,280
Attorney for Applicant

JFH/pmp

BAKER & DANIELS
111 East Wayne Street, Suite 800
Fort Wayne, IN 46802

Date: February 19, 2002

10/049952

JC10 Rec'd PCT/PTO 19 FEB 2002

1

SKULL CRUCIBLE FOR MELTING OR REFINING INORGANIC SUBSTANCES

The present invention relates to a so-called skull crucible for melting or refining
5 inorganic substances, in particular glasses and glass ceramics.

Such crucibles comprise a crucible wall which is generally cylindrical and is made
up of a crown of vertical metal tubes, with slots between adjacent tubes. The
crucible base may be composed of metal tubes, yet it can also comprise fireproof
10 material. Said tubes are connected at their ends to vertical tubes for supplying or
draining off coolant.

Heating is effected by an induction coil surrounding the wall and via which high
frequency energy is coupled to contents of the crucible.

15 A skull crucible for melting inorganic substances is disclosed in EP 0 528 025 B1,
for example.

A skull crucible functions as follows: the crucible is filled with heterogeneous
20 mixture or flakes or a mixture hereof. The glass or the melt must first be preheated
to obtain a certain minimum conductivity. Preheating often occurs by burner
heating. If the coupling temperature is reached more energy can be supplied by
irradiation of high-frequency energy. During operation also the melt can be heated
additionally for heating by means of high-frequency energy via burners which have
25 an effect on the melt from above, or via hot waste gases.

During operation an edge layer of solidified melt forms on the cooled crucible wall
comprising metal pipes. A layer of crystalline material is advantageous here which
has better heat insulation as compared to a vitreous layer. The edge layer protects
30 the crucible wall from corrosion by aggressive or hot melts. This cold edge layer is
vitreous or crystalline depending on glass melt.

The base layer is also cold, since the base is likewise cooled, similarly to the peripheral walls, where a vitreous or crystallised cold base layer also forms. This is a disadvantage for pouring out the melt via a base run-off. To let the melt run out through the base run-off, the solidified base layer must be loosened either by being knocked or dissolved thermally by means of additional heating units. The resulting effect of such a crystalline layer for the melt flowing past is a nucleating agent, and this is undesirable. In addition, the HF field is weaker in the base region, as the coil terminates ca. 2-5 cm above the base.

10 The high-frequency energy can be utilised only for heating the interior of the skull crucible. On the other hand it cannot be employed for specific heating of the cooled base region. If the aim were to heat the layers close to the base using induction heating, then heat would be drawn from these layers again by cooling of
15 the base. This would culminate in impoverishment of the energy introduced, compared to the uncooled hot middle zone of the melt.

20 It might also be conceivable to increase the high-frequency energy overall so that the temperature of the base region exceeds the upper devitrification temperature. In that case the problem of decanting would have to be overcome. But the melt in the central region of the skull crucible would then be superheated. This could lead to synthesis by selective vaporising being displaced, resulting in fluctuations in refractivity and lubricating.

25 There is little literature on special techniques of the discharge of glass melt from a skull crucible. In general a run-off opening is illustrated diagrammatically only. US 5 567 218 describes an outlet opening which is cooled only slightly and is relatively large, and to which a well cooled slide is assigned. At the same time a short ceramic sleeve projects into the melt whose sole task is to thermally insulate the run-off area to facilitate run-off. This reference also makes mention of variants
30 with indirect heated discharge feeders.

Were these embodiments which are insensitive to crystallisation or slightly sensitive adequate for such melting, then their disadvantage is that the meltings contain a large number of crystals and streaking after run-off. With optical
5 crystallisation-sensitive melting crystals form during such run-off on the abovementioned ceramic sleeve. These impair removal of the melt from the base region. They also disallow controlled discharge. The discharge rate cannot be especially well controlled. In the case of aggressive glasses there is the added risk that the ceramic sleeve is rapidly melted and that the dissolution products cause
10 flaws in the glass.

The object of the present invention is to provide a skull crucible of the type initially described, such that also with problematic glass types the melt can be discharged from the base region in a controlled fashion, without impairment of the glass
15 quality, particularly with aggressive or qualitatively high-quality glasses.

This task is solved by the characteristics of Claim 1. The inventors have recognised that there is the possibility of trouble-free removal of the melt if measures are put in place to remove melt from the hotter zones only. The cold,
20 crystallised glass of the base region is therefore not to be removed according to the invention.

This ensures that no crystalline material from the base region reaches the ingots, that during the casting process the melt does not pass by the crystallised base
25 layer and accordingly new nuclei constantly do not form and get carried along and that devitrification products of higher density than the glass melt itself, which are deposited in the base region, is not drawn into the ingot. Also, the run-off sleeve can be of such a diameter and length corresponding to viscosity of the melt that a laminar discharge of the melt without turbulence in the mould is ensured. This
30 technique can be used to manufacture crystal-free and streak-free ingots from optical glass

The invention offers another advantage: with discontinuous crucible melting no stoppage of the glass flow is necessary; rather the glass flow stops itself, as a result of intelligent height selection of the sleeve. The residual gas remaining in the
5 crucible ensures further HF coupling.

Accordingly, the process can immediately be continued. At the same time new heterogeneous mixture can be replenished without renewed processing by way of additional heating, for example by means of a burner flame.
10

This is a particular advantage with glass types of minimal conducting capacity, which are difficult to connect, as well as with glass types having readily volatile batch constituents which vaporise or atomise strongly when burner heating is employed.
15

Two platinum variants were tested as embodiments. Common to both variants is the fact that the discharge pipe and the sleeve comprise platinum or a platinum alloy and the discharge pipe is fitted with a 50 Hz resistance heating unit. Platinum is used accordingly because it is stable under oxidising conditions up to 1600°C
20 and barely causes traces of discoloration in the glass. For higher temperatures sleeves made of iridium, molybdenum and wolfram or compounds of these materials are suitable.

According to a first variant the run-off pipe ideally has a height of ca. a third of the overall melt level, if at the same time it is to be ensured that coupling is also to be guaranteed during and after casting. If there is not this requirement then due to contamination of the melt by the material of the platinum sleeve it is more favourable to have the sleeve considerably shorter. Sleeves of 2 to 6 cm long have proven suitable for this. The glass seal between platinum flange and water-cooled
30 skull crucible is ensured by a quartz plate as well as ring air cooling around the platinum flange. According to melt and corrosion requirements the quartz ware

plate is between 1 and 2 cm thick. And in all cases the platinum sleeve must project at least 1 cm above the quartz ware plate.

In the second variant the structure for extreme demands on platinum freedom was further optimised. In this case the platinum sleeve is cooled with air during melting and refining. This ensures that during these melting phases the platinum is separated by a solid glass layer from the melt and no dissolving can take place. Just before the casting phase cooling is reduced or turned off completely and the glass on the platinum sleeve is heated to a temperature above the devitrification limit. When all crystals in the vicinity of the discharge are dissolved the 50 Hz resistance heating of the platinum pipe is raised to casting temperature and the melt is removed. When the glass limiting layer is dissolved the temperature can be determined by measuring it using a thermoelement attached to the sleeve.

The thermoelement is withdrawn via the gas outlet from the cooled sleeve and conveyed via feedthrough capacitors to a measuring unit. The feedthrough capacitors assist in filtering or smoothing possible HF interference signals.

The platinum run-off sleeve could on principal also have contact with the water-cooled skull crucible from an electrical layer. But this variant does have drawbacks relative to cooling, as in this case the platinum run-off is influenced by the water cooling of the skull crucible and thus there is the danger of excessive cooling in the vicinity of the run-off sleeve. For very aggressive glass melting this variant can be advantageous though, since in this case the problem of glass sealing between skull and platinum run-off sleeve does not apply.

Electrical uncoupling of flange and metallic skull crucible is desirable whenever glass sealing is not problematic. This leads to a lower HF interference level on Pt heating. In the event of electrical uncoupling of flange and metallic skull crucible there must be a distance of at least 0.5 cm between both components, which is filled with electrically insulating ceramic. The best material here is quartz ware.

Another conceivable run-off variant would be a quartz glass pipe which projects a few centimetres into the melt in the upper region and is heated indirectly below the crucible base. The advantage to this variant is absolute platinum freedom of the melt. The drawback is the limited stability of the run-off in particular due to corrosion by aggressive glass melting.

Embodiment:

A glass from the Lanthan Krone family was melted and cast. The HF energy is supplied via a generator with a frequency of 1 MHz. The melt volume is ca. 8 l. The melt level in the skull crucible was 21 cm. The HF energy required for casting is 30 kW. The upper devitrification temperature of the glass is ca. 1040°C. The casting temperature is 1100°C. At this target temperature the temperatures in the centre of the crucible between base, middle and surface fluctuate between 1000°C at the base, 1150°C in the middle and 1100°C in the vicinity of the melt surface. This means that a crystal layer, which due to the sleeve construction does not have an adverse affect, is on the base during casting.

A platinum run-off pipe 50 cm in length, a pipe diameter of 8 mm and a fitted sleeve 10 mm in diameter and 7 cm sleeve length were used. The platinum tube has a flange mounted in the region of the crucible base, which is set directly on the alumosilicate base plate of the skull crucible and which assists in attaching the heat circuit. The distance between flange and water-cooled skull crucible is 5 mm. The flange edge at the top is air-cooled. In the case of highly corrosive glass melting or high refining temperatures the switch can be made from air cooling to water cooling, as required. Located at the lower end of the platinum pipe is another plate lug for laying on power to heat the flange. The platinum flange can be heated by means of a heating circuit between flange and plate lug to temperatures up to a maximum of 1400°C. Only the pipe itself is heated, whereas the sleeve projecting into the glass is heated only indirectly by thermal conduction from the platinum tube and from the hot melt.

During melting and refining the platinum run-off pipe is unheated. Around 1 to 2 hours prior to casting the crucible is set to casting temperature and the platinum flange is also slowly brought up to casting temperature. When the target
5 temperature is reached both for the melt and the run-off the glass warms up.

When the air-cooled sleeve is used the air cooling on the sleeve is turned off to additionally adjust the target temperature on the pipe and in the melt for casting. The glass is held back by a stopper at the warm-up stage, until all target
10 temperatures have been reached and the temperature on the sleeve is above 1050°C, thus clearly above the upper devitrification limit.

The invention is now explained in greater detail with reference to the diagram, in which:

15 Figure 1 illustrates a skull crucible according to the first variant in diagrammatic vertical section.

20 Figure 2 illustrates a skull crucible according to the second variant in a diagrammatic vertical section.

The skull crucible 1 illustrated in the figures serves to melt or refine inorganic substances, in particular glass or glass ceramic, and especially broken glass or so-called heterogeneous mixtures or both.

25 The skull crucible has a wall 1.1, formed by a crown of vertical metal pipes which are conductively connected to one another and are attached to a coolant, such as water.

30 The base 1.2 of the skull crucible 1.1 is constructed from a quartz ware plate. It, too, is cooled, especially by air exiting from pipes 1.3.

The wall 1.1 is enclosed by an induction coil 2. This is a component of a high-frequency facility, with which high-frequency energy is supplied to the contents of the skull crucible.

5

As can be seen, a melt 3 is inside the skull crucible. The wall 1.1 and the base 1.2 of the skull crucible 1.1 are each covered by a crystallised layer 3.1, 3.2. Coring products 3.3 are illustrated schematically in the base region. These can form in certain glass types, and sink down to the base from the interior of the melt.

10

According to the invention a platinum sleeve 4 is provided as run-off. The upper edge 4.1 of the sleeve 4 clearly projects out over the upper edge of the base 1.2. The upper edge is located in a zone lying far above the crystallised base layer, where the temperature is clearly above the devitrification temperature. Due to the position of the upper edge 4.1 there is no danger of the coring products 3.3 reaching the sleeve 4 and impair the quality of the removed glass melt.

15

The skull crucible 1 according to Figure 2 is fundamentally of the same structure as that according to Figure 1. It too has a sleeve 4 for removing glass melt. The upper edge 4.1 of the sleeve 4 is again located in a relatively hot area of the glass melt.

20

Compared to the embodiment of Figure 1 however a cooling system is provided which is assigned to that area of the sleeve 4 located inside the melt 3. This cooling system exhibits a mantle 4.2 which encloses the upper area of the sleeve 4. Formed between mantle 4.2 and the upper area of the sleeve 4 consequently is a cavity which has an inlet 4.3 and an outlet 4.4. Attached to the inlet 4.3 is a coolant, such as a gas. A thermoelement 4.5 is provided in the cavity.

25

When the skull crucible is operating it is generally effective to regulate the temperature of that part of the sleeve projecting into the melt 3 such that the

30

temperature of the sleeve 4 is kept low during the melting phase. At the same time the temperature should be low enough to allow a solid glass or crystal layer to form, and when the melt is being drawn off the value of the temperature is raised above the upper devitrification point.

5

It can also be effective to keep the base region of the skull crucible at a temperature level lower than the superjacent glass melt. The advantage here is that there is less corrosion of the base.

10

Claims:

1. A skull crucible (1) for melting or refining inorganic substances, in particular
5 glass or glass ceramics;

1. 1.1 with a crucible wall (1.1);
2. 1.2 with a crucible base (1.2);
3. 1.3 with an induction coil (2) surrounding the crucible wall (1.1) wall and via
10 which high frequency-energy is coupled to contents of the crucible;
4. 1.4 the crucible wall is formed from a crown of metal tubes which can be
connected to a coolant, with slotted interstices between adjacent metal
tubes;
5. 1.5 the base (1.2) has a run-off for the melt;
6. 1.6 a sleeve (4) is assigned to the run-off;
7. 1.7 the inlet end (4.1) of the sleeve protrudes into the inner chamber of the skull
crucible (1) so that the melt can be removed through the crystallised base
layer in a controlled manner without the danger of impairing its quality.

20 2. A skull crucible as claimed in Claim 1, characterised in that the upper edge
of the sleeve (4) is at a height of between a tenth to a half of the melt height
measured from the base (1.2) of the crucible.

25 3. A skull crucible as claimed in 1 or 2, characterised in that the sleeve (4) is
assigned a device for adjusting or regulating its temperature.

30 4. A skull crucible as claimed in Claim 3, characterised in that the upper area
of the sleeve (4) projecting into the melt and forming a cavity is double-
walled, and in that the cavity has an inlet (4.3) and an outlet (4.4) for a
coolant.

5. A skull crucible as claimed in any one of Claims 1 to 4, characterised by the following features:

1. 5.1 the sleeve (4) has two coaxial sleeves;
- 5 2. 5.2 the outer sleeve is a metal jacket;
3. 5.3 the inner sleeve is a quartz glass tube.

10 6. A skull crucible as claimed in any one of Claims 1 to 5, characterised in that the sleeve is height-adjustable.

DIN

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1. März 2001 (01.03.2001)

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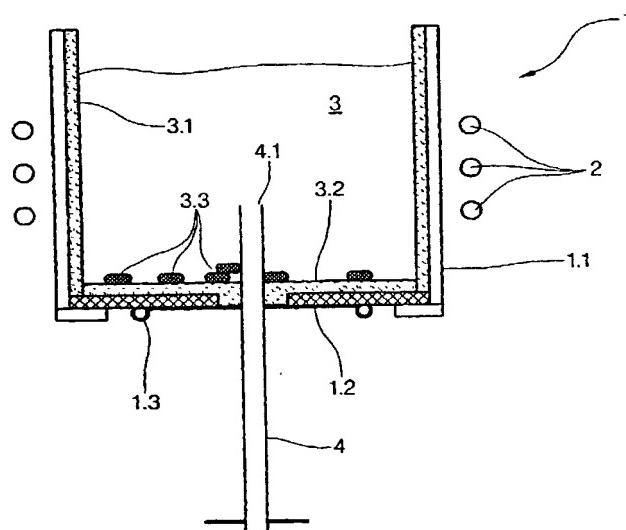
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- (51) Internationale Patentklassifikation⁷: C03B 5/26,
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55122 Mainz (DE).
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ZW): CARL-ZEISS-STIFTUNG trading as SCHOTT
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[Fortsetzung auf der nächsten Seite]

(54) Title: SKULL POT FOR MELTING OR REFINING INORGANIC SUBSTANCES, ESPECIALLY GLASSES AND GLASS CERAMICS

(54) Bezeichnung: SKULLTIEGEL FÜR DAS ERSCHMELZEN ODER DAS LAÜTERN VON ANORGANISCHEN SUBSTANZEN, INSbesondere von GLÄSERN UND GLASKERAMIKEN



(57) Abstract: The invention relates to a skull pot (1) for melting, crystallising or refining inorganic substances. Said pot comprises a pot wall (1.1), a pot bottom (1.2), an induction coil (2) which surrounds the pot wall (1.1) and by means of which high-frequency energy can be coupled into the content of the pot. The pot wall (1.1) is formed by a ring of metal pipes which can be connected to a cooling medium. Slits are embodied between adjacent metal pipes. The bottom (1.2) is provided with a discharge for the melt (3). A sleeve (4) is allocated to the discharge. The admission end (4.1) of the sleeve (4) protrudes far into the inner chamber of the skull pot (1) in such a way that, during use, the melt (3) can be withdrawn through the crystallised bottom layer (3.3) in a controlled manner without the danger of impairing quality.

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Fig.1

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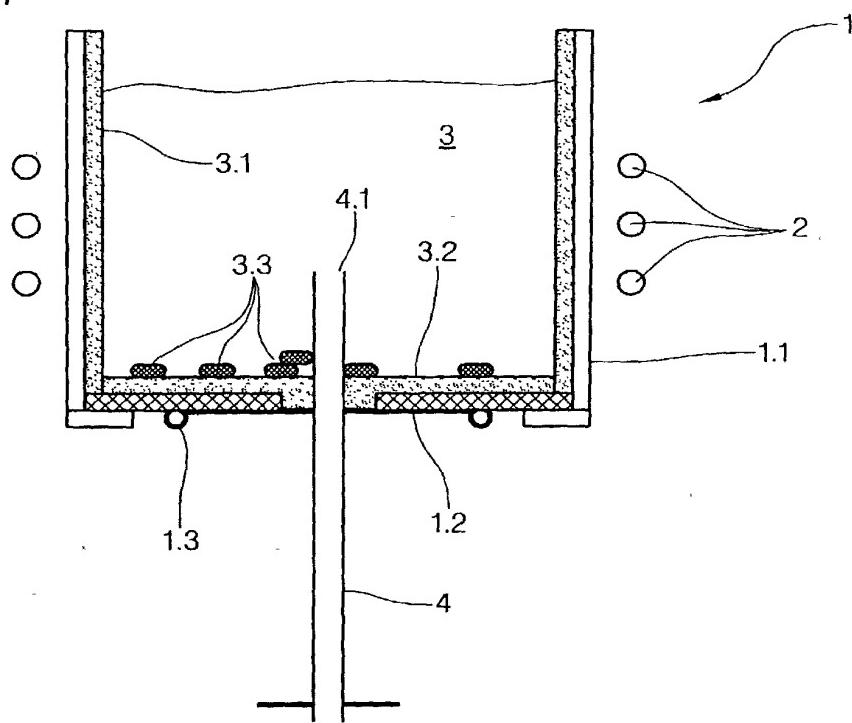
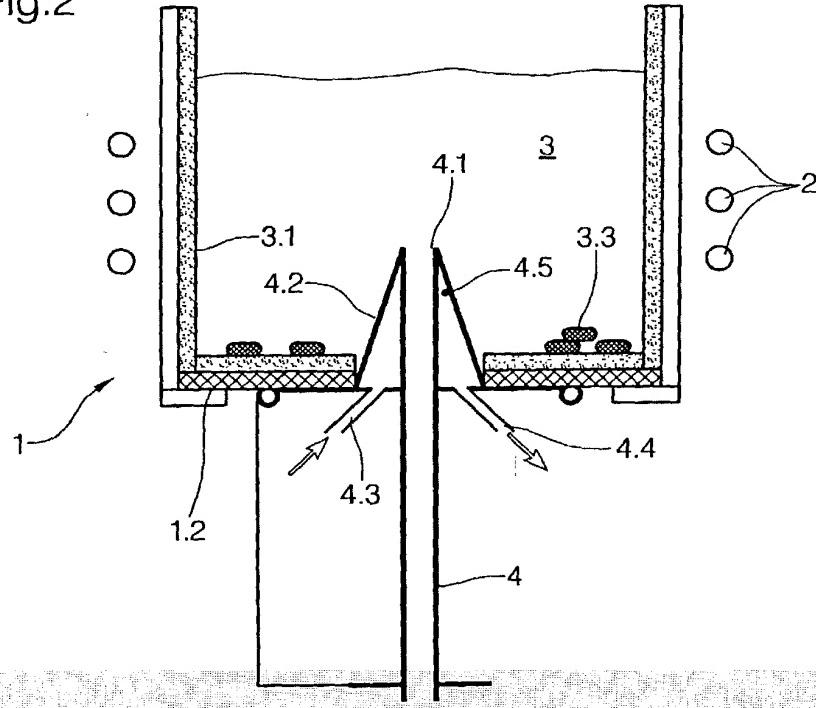


Fig.2



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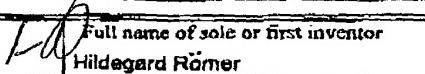
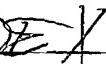
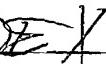
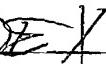
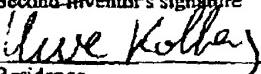
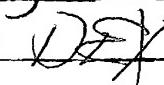
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